



Well #6

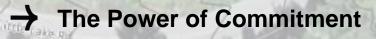
Well Siting Study

Drought Tolerance Emergency Water Supply and Storage Improvements

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Mendocino City Community Services District Drought Tolerance Emergency Water Supply and Storage Improvements

March 29, 2023



Well#

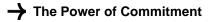
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NOTE: This study was developed utilizing common engineering and hydrogeologic resources and with information provided by the Mendocino City Community Services District, the Mendocino Unified School District and from previous studies. Engineering judgment was applied where appropriate. Future conditions may vary from those predicted in this study. All recommendations should be validated and adjusted as appropriate during the design and construction process. Due to periodic changes to regulations, procedures, design guides, and policies, the potential solutions and recommendations contained herein may be subject to revision.

1. Introduction

1.1 Purpose of this report

GHD Inc. (GHD) was engaged by the Mendocino City Community Services District (MCCSD) to prepare this well siting study, which follows up on the conclusions and recommendations of a hydrogeological investigation of groundwater availability prepared by GHD in January 2023 (GHD, 2023) and previous studies published by GHD in 2019 and others for the Mendocino Unified School District (MUSD) wellfield and the immediate vicinity. Additionally, this study reviews and summarizes a previous MUSD Well Siting Study (GHD, 2019) and brings it into the context of this project's goals and objectives. The purpose of the information provided herein is to ultimately support the environmental review, siting, and final design of a new well field consisting of up to ten water supply wells within the MUSD property accessed from Little Lake Road. This scope of work supports the Drought Tolerance Emergency Water Supply and Storage Improvements project that is jointly supported by the MCCSD and MUSD and funded by the California Department of Water Resources Urban and Multibenefit Drought Relief Grant program and California Water Resources Control Board Proposition 1 Drinking Water State Revolving Fund Planning and Construction Grants.

The project Site is located on a MUSD owned parcels located north of the K-8 School campus. The wells are located on one parcel (APN 119-100-03) that is accessed from Little Lake Road and located west of the school's existing supply wells and storage tanks, shown in Appendix A, Figure A. The Site consists of only the single parcel and does not include the adjacent parcel to the east where the construction of replacement water tanks and a treatment and control building is planned. The proposed locations of the well field are shown in Appendix A, Figure A.

The project proposes to develop additional water supply and provide additional water storage to assist the Village of Mendocino in meeting daily water demands during drought conditions and minimize the need to import water from outside the area. Water would be stored in and accessed from the MUSD water system, which serves the K-8 School, Mendocino High School, Friendship Park and the Mendocino Community Center. The purpose of this study is to review potential locations for a secure, reliable, high-quality potable water supply to add to the MUSD system as a new emergency and back-up water source during drought conditions and for long-term water source resiliency for the Village of Mendocino. This study includes a review of:

- Current Groundwater Conceptual Model. Local aquifers.
- **Site Conditions**. A summary evaluation was developed based largely on existing/previous studies and regional information.
- Existing Well Construction. Summarizing the existing potable water sources (MUSD Wells #1, #2, & #6) construction, repairs, and water quality data was reviewed to understand deficiencies of the system and how new supply wells could be feasibly sited, constructed, and integrated into the system.
- **Historical Water Usage**. Timeline records were reviewed and summarized to determine the need for a new well.
- Site Screening Criteria. Opportunities for Site locations were evaluated.
- **General Findings** and **Conclusions and Recommendations** were developed based on this and previous studies of the Site and area.

1.2 Scope and limitations

This report has been prepared by GHD for the Mendocino City Community Services District Drought Tolerance Emergency Water Supply and Storage Improvements and the Mendocino Unified School District and may only be used and relied on by Mendocino City Community Services District Drought Tolerance Emergency Water Supply and Storage Improvements and the Mendocino Unified School District for the purpose agreed between GHD and Mendocino City Community Services District Drought Tolerance

Emergency Water Supply and Storage Improvements and the Mendocino Unified School District as set out in Section 1 of this report.

GHD otherwise disclaims responsibility to any person other than Mendocino City Community Services District Drought Tolerance Emergency Water Supply and Storage Improvements and the Mendocino Unified School District arising in connection with this report. GHD also excludes implied warranties and conditions, to the extent legally permissible.

The services undertaken by GHD in connection with preparing this report were limited to those specifically detailed in the report and are subject to the scope limitations set out in the report.

The opinions, conclusions and any recommendations in this report are based on conditions encountered and information reviewed at the date of preparation of the report. GHD has no responsibility or obligation to update this report to account for events or changes occurring subsequent to the date that the report was prepared.

The opinions, conclusions and any recommendations in this report are based on assumptions made by GHD described in this report. GHD disclaims liability arising from any of the assumptions being incorrect.

1.3 Assumptions

This report summarizes information from the MCCSD, the MUSD, and previous studies by GHD and other information about a new well field proposed to be located on MUSD property which will be subject to review by the MCCSD, the MUSD, the County, State, and others.

Changes to the report will be made in part based on comments and feedback from reviews.

Recommendations for the new well field are preliminary and final locations may be updated based on additional data collected during test well installation anticipated in 2023, and feedback received from MCCSD, MUSD and other stakeholders.

2. Desktop Review

2.1 Previous results/conclusions of GHD 2019 MUSD Well Siting

GHD previously conducted a series of studies for MUSD for future additional production capacity and source water supply resiliency. These included a source water well inspection and specific capacity testing study (GHD, 2019b), a well siting study (GHD, 2019c), a test well drinking water source assessment and protection and water quality study (GHD, 2020), and constructed of a new test well (MUSD Well #6) with pump and specific capacity testing (GHD, 2021). The MUSD currently operates two active wells (Well #1 and Well #2) at the Site that will remain operational during the construction and implementation of the proposed well field.

In addition to previous GHD studies, numerous hydrological studies were performed in the 1980s through at least the early 2000s by Don Clark Engineering and Hydrology, and other regional firms. Hard copies were reviewed by GHD as provided by several domestic well owners downgradient to the MUSD.

2.1.1 Summary of MUSD 2019 Well Siting Study

GHD previously prepared a Well Siting Study (2019) supporting the construction of MUSD Well #6. The study included two areas that are located within the project boundaries of this project Site A and Site B with Well #6 being located inside Site B, as shown in Figure 1 below.



Figure 1 GHD 2019 Well Siting Study - Figure 3

A summary of Site A and B screening results for Well #6 are provided below:

Site A

- The anticipated shallow marine terrace materials here would be comparable to, and slightly thinner than, that of the Well #1 and Well #2 locations, resulting in an above average water yield for the area (based on available well completion reports in the vicinity);
- Water quality (relatively good) is anticipated to be comparable to that of Well #1 and #2, however, it is unclear how close the residential septic system to the west would be to the final well Site here and how much temporary noise mitigation would need to be considered;
- There is ample room to move around to the exact location of the test well (Well #6) away from any potential wetlands, springs, or other CEQA considerations;
- The property is owned by MUSD and access to a location here would be good; and,
- The Site is generally clear of overhead power lines and is relatively close to the existing and future water supply lines, the water treatment and control building, and storage tanks. Overall, this is a good potential Site for consideration of a test well. Although there are no major issues, temporary noise mitigation measures for adjacent residences and wetland setbacks may be necessary.

Site B

- The anticipated shallow marine terrace materials here would be comparable/equivalent to that of Well #1 and Well #2, resulting in an above average water yield for the area (based on available well completion reports, Appendix B); water quality (relatively good) is anticipated to be comparable to that of Well #1 and Well #2;
- There is decent room to move around the exact location of the test well (Well #6) away from any potential wetlands, springs, or other CEQA considerations;
- The property is owned by MUSD and access to a location here would be good; and,
- The Site may need some tree limb work prior to well construction, but is generally clear of overhead power lines and is very close to the existing and future water supply lines, the water treatment and control building, and storage tanks.

2.2 Background Summary

2.2.1 Site Conditions

The Site is located approximately 1 mile east of the Pacific Ocean on the Mendocino Headlands, on the outskirts of the Village of Mendocino. The Mendocino Headlands consist of a series of relatively flat terraces that form benches into the surrounding bedrock. The headlands protrude approximately 1/5 mile into the Pacific Ocean and terminate with nearly vertical cliff faces that generally extend between 40 and 60 feet above sea level.

The Site is situated on the north side of Little Lake Road, approximately 0.7 miles east of the intersection of Little Lake Road and State Route 1 at an elevation ranging from 385- to 425- feet NAD88. The Site slopes to the west at a consistent 10 percent grade and is heavily forested throughout with exception to the southwest corner where there is an existing MUSD maintenance building and driveway that leads east to the existing MUSD wells and water tanks.

The Site is located on Pleistocene aged marine terrace deposits that are underlain by Franciscan Complex Coastal Belt (Franciscan bedrock). A relatively shallow organic soil horizon overlays the terrace deposits that range from 1- to 4-feet in depth. Marine terraces represent former beach and near shore environments and consist of silty sand that form essentially flat stratigraphic surfaces that cover the underlying Franciscan bedrock (DWR, 1985). There are four primary marine terraces that have been documented by Todd and others that constitute the Mendocino Headlands marine terrace aquifers aquifer:

- **Casper Point**: Occurs between elevation of 40- to 80-feet elevation and is the youngest marine terrace (approximately 100,000 years old). The terrace is composed of medium-grained loose sand with few fines and is generally about 10 feet thick.
- Jughandle Terrace: Occurs between 80- to 160-feet elevation and is the second youngest marine terrace (about 200,000 years old). The terrace is composed of fine-grained silty sand and is generally about 20 feet thick with a maximum thickness of 35 feet.
- **Railroad Terrace**: Occurs between 160- to 200-feet elevation and is the third youngest terrace (about 300,000 years old). The terrace is composed of fine-grained sand with a higher percentage of silt and clay than the younger terraces.
- Fern Creek Terrace: Occurs between 300- to 400-feet elevation and is the oldest documented marine terrace (about 400,000 years old). The terrace is composed of fine-grained silt and clayey sand and is generally up to 15 feet thick.

Franciscan bedrock consists of interbedded greywacke sandstone and shale that is pervasively fractured. The bedrock holds very little potential for water storage however the fractures allow for groundwater storage and transmissivity and generally understood to decrease with depth and distance from the coastline (DWR, 1985).

The Site is located beyond the traditionally mapped extent of the Fern Creek Terrace, located approximately ¼ mile southwest. Nearby well completion reports indicate that the alluvial thickness on the western half of the Site is similar to that of the Fern Creek Terrance (around 15 feet) however there is a grade break that increases the elevation by approximately 30 feet which directly translates to increase of the marine terrace thickness to approximately 50 feet. This increase may be an extension of the Fern Creek Terrace or part of an unknown older and unmapped marine terrace.

The primary method of recharge for the aquifer is precipitation infiltration with excess surface runoff flowing into creeks and ultimately the Pacific Ocean to the west. Areas that have exposed bedrock tend to have poor infiltration rates resulting in the alluvial and marine terraces being primary recharge and storage areas. Due to the topographic setting of the Mendocino Headlands, a major portion of the annual groundwater outflow is through shallow springs along the surrounding cliffs resulting in the shallow aquifer(s) having reduced long-term storage capacity and influenced by the annual weather patterns much more than typical California inland valley alluvial aquifers.

Topography and groundwater flow indicate that surface and groundwater flow is northwest towards Slaughterhouse Gulch and is hydraulically disconnected from the Big River Watershed located south of the Village of Mendocino.

Briefly developed here from this study and review of previous studies, is a general hydrogeological conceptual model (HCM) for groundwater underlying the Project Site and the immediate vicinity aquifers downslope. This is intended to aid in the siting and design of the proposed well field and for future surface and groundwater monitoring protocols. This should be considered preliminary and should be updated as future groundwater monitoring data is collected. Directly below the study area (MUSD) and to the west are three principal aquifer types – marine terrace aquifers, alluvial aquifers, and Franciscan bedrock aquifers.

<u>Marine Terraces</u> - An older marine terrace of up to 50-feet thick occupies the MUSD parcel and transmits relatively shallow groundwater within an unconfined aquifer with water levels ranging in depth of approximately 15 to 30-feet (seasonally and precipitation dependent) that flows to the west. Three existing MUSD wells are constructed up to 50-feet deep and have the highest relative specific capacities and long-term yields in the nearby area, ranging from approximately 6 to 9-gpm. These wells also have the most potential to hydraulically interfere with each other if pumped simultaneously.

The old marine terrace thins to the west and a few springs and wetlands emerge downslope where the marine terrace has been naturally eroded from surface water incision and bedrock is correspondingly encountered at shallower depths. Bedrock seasonally forces groundwater to the surface of the marine terrace, as evident in the springs located west of the MUSD water tanks and east of the MUSD maintenance building. These springs represent a portion of the Slaughterhouse Gulch headwaters and its first seasonal surface flows in the immediate area. Another distinct spring fed branch to Slaughterhouse Gulch begins offsite approximately 1,000-feet to the northwest on the northeast portion of Gurley Lane. The two spring systems flow westerly downslope and converge near Calypso Lane to form the defined Slaughterhouse Gulch stream, with year-round surface flows even during periods of drought.

<u>Alluvial (creek) Deposits</u> – Creek deposits are generally less than 20-feet in thickness and have formed from overland flow incising and eroding the various marine terraces. This is shown in neighboring large diameter (3-feet) concrete caisson wells, downgradient of the Site installed adjacent to Slaughterhouse Gulch, which are generally less that 20-feet deep and used for both irrigation and domestic supply purposes. The relatively thin and shallow alluvial aquifers have developed from the deposition, erosion, and redepositing cycle of those sediments along the creek banks and gulches as the surface water has migrated westerly to the Pacific Ocean over time. Creek alluvial groundwater flow is generally directly connected with the surface water in Slaughterhouse Gulch and thus this groundwater type is most vulnerable to seasonal variations in precipitation and droughts. The alluvial groundwater is a very shallow; near the ground surface unconfined aquifer that ranges from approximately 5 to 15-feet in thickness.

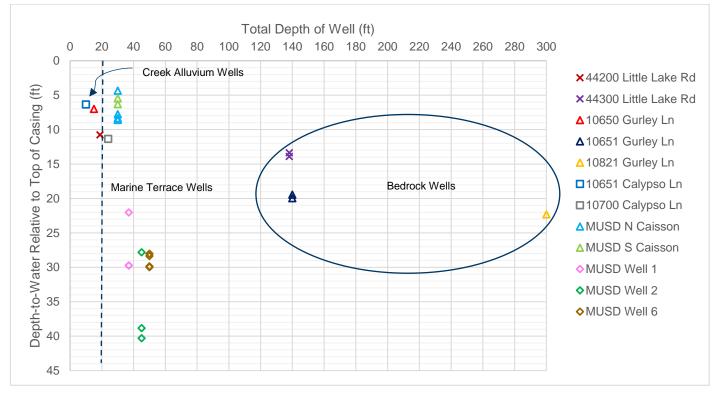
Bedrock - The Site and lower elevation marine terraces and alluvial terraces are underlain by Franciscan hard rocks of graywacke to slatey materials of relatively low to very low permeability and transmissivity and contain variable groundwater aquifers that move via fracture flow. The Franciscan rocks have variable long-term yields in wells, ranging 0.1 to 3-gpm in near vicinity wells (up to 10 gpm in the wider Mendocino Headlands area), have variable to unknown total depths of groundwater, have a relatively low storage potential, and are recharged much more slowly by the overlying marine and alluvial terraces over longer periods of time. Bedrock completed wells generally range from 100 to 300-feet or more in depth, and likely exhibit mostly confined to semi-confined conditions.

2.2.3 Existing Well Conditions

Previous manual depth-to-water measurements were taken from top of casing (TOC) of surrounding public and private wells (GHD, 2023). The TOC varied for each well but in general were less than 2 feet above the ground surface. Figure 2 shows the depth-to-water measurements relative to the total depth of each well.

Water levels around the project area range from 4 feet to 40 feet below ground surface with wells in the shallow terrace deposits having water levels around 5 to 10 feet below TOC and bedrock wells having water levels around 15 to 20 feet below TOC. The exceptions to this are the three MUSD wells (Well #1, Well #2, and Well #6) which have water levels between 20 and 40 feet below their respective TOC. This could be due to their much more active use compared to the other wells and within a higher elevation marine terrace that is not directly hydraulically connected to

the lower elevation wells within different formational types (alluvium and bedrock). Transducer recordings from September 29th to November 24th are shown in Figure 3.





Depth-to-Water vs Total Well Depth of Nearby Wells

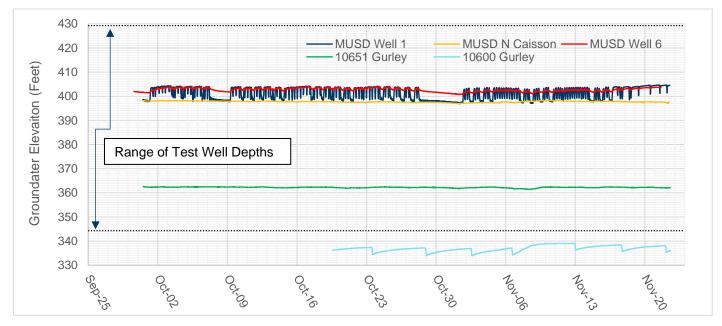


Figure 3 Well Transducer Data September 29th – November 24th 2022

Based on the collected transducer data the total range of the proposed well field would potentially only draw from the same aquifer as the MUSD wells since the 10651 Gurley well is a bedrock well and the bottom elevation of the lowest potential new well is above the recorded water surface elevation of the 10600 Gurley well.

2.2.4 Historical Water Use

Pumping data provided by MUSD is shown in Figure 4 and dates to 2017, showing the stable combined average flow rate from the wells. Production from Well #1 and Well #2 ranges from 6 to 8 gallons per minute with an average of 6.8 gallons per minute. Well run times for Well #1 and Well #2 are generally synchronized and are operational for an average 4-5 hours per day with Well #1 being run for slightly less time than Well #2.

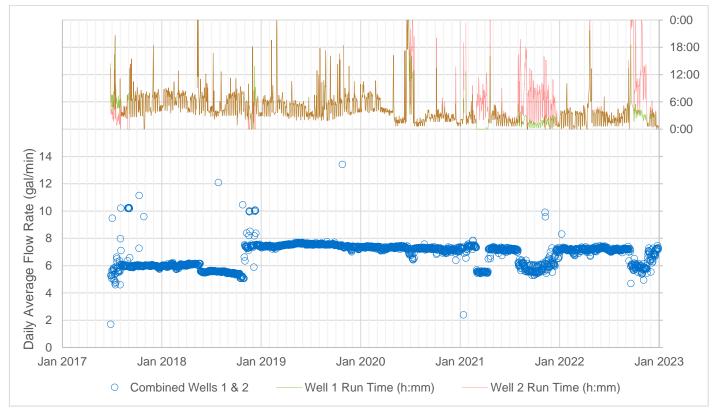


Figure 4 Pumping Statistics from MUSD combined Well #1 and Well #2

3. Site Screening Criteria

The project Site consists of a single parcel, shown in Appendix A, Figure C. Based on the variable aquifer thickness across the Site, the parcel has been divided into three zones based on surface elevation. Surface elevations across the Site range from 430 feet to 380 feet: Zone A is for elevations above 420 feet, Zone B is for elevations between 420 feet and above 400 feet and Zone C is for elevations below 400 feet.

The current Site uses were reviewed through previous and recent discussions with MUSD, site visits, review of surrounding parcels available information. All areas within the parcels were considered as part of this well siting study. Improvements on the parcels include the maintenance building, water supply wells, water storage tanks, the treatment and control building, and the gravel/dirt driveway. Additional improvements include a radio antennae attached to a tree and a small communications shed used for the student radio station, along with various wood and maintenance equipment storage and staging areas.

Ranking of potential well locations considered hydrogeological details as well as surrounding land use, proximity to existing infrastructure, property availability, restrictions, environmental issues, accessibility and public concerns.

Available data together with GHD's professional judgement were used evaluate then rank the sites with the highest potential to yield a reliable, redundant, long-term water supply by using the screening criteria. The potential sites were scored with respect to five screening criteria as outlined in the section below. The resultant scores for each of the criteria were totaled to generate a ranking of potential locations relative to each other. MCCSD generally expects to test drill at the best candidate sites and potentially convert those borings into a series of wells in an overall wellfield at the Site.

3.1 General Findings Criteria

This section briefly describes the criteria and general findings used to rank potential sites. Information was reviewed to support this well siting with these criteria:

- Water Quantity (Anticipated Yield) 30 points Since this particular area is generally considered a low yielding water production area, water quantity is the most heavily weighted and important selection criteria. Subsurface hydrogeology has significant influence on the quantities of water that can produced on any given location.
- Water Quality 20 points Included in this criterion is naturally occurring constituents like iron, arsenic, manganese, and human related constituents like gasoline, motor oil, septic by-products, and nitrates. Minimized treatment of high-quality water prior to conveyance is preferred.
- Environmental Considerations 20 points Potential impacts to the environment from well drilling and conveyance piping construction, effects on vicinity wells and California Environmental Quality Act (CEQA) considerations are included in this criterion.
- 4. Well Construction Logistics and Engineering Feasibility 15 points This criterion includes available accessibility, lateral and overhead drilling space, ease of water discharge during well development and pump testing.
- 5. Cost 15 points Relative costs to develop a well at each potential site were considered in this criterion including site proximity to the treatment building and storage tanks, pipeline lengths to conveyance connections, construction mitigation considerations, public perception, and aesthetics.

3.2 Water Quantity

This section summarizes the information in record searches and from GHD's institutional knowledge and previous work conducted in the project area to summarize potential groundwater development based on local geology, hydrogeology, groundwater yields, and available site data. A high-ranking site for groundwater quantity should be situated on a relatively productive groundwater aquifer(s), have a significant area of groundwater recharge, and located away from other supply wells in the area to avoid well interference problems.

The site is located in the Fort Brag Terrace Area Groundwater Basin 1-021 and the hydrogeology of the immediate vicinity can generally be broken into two categories: first water bearing zone/aquifer of near surface (from approximately 0-50 feet below the ground surface) sediments consisting primarily of marine terrace deposits that have a wide range of reported yield (1-100 gpm); and, Franciscan Formation bedrock (from approximately 0-30,000 feet below the ground surface) aquifer consisting of fractured (variably) greywacke sandstone and turbidite sandstone (often called shale by drillers) sequences, with localized serpentinite. The Franciscan bedrock in the area is considered a very low to low yielding aquifer media in the area (0.1-10 gpm).

The marine terrace deposits on MUSD property range from 0 to 50-feet bgs and are likely thickest in the eastern portion of property and tapers down going west across the property (See Appendix A, Figure C). MUSD water supply data and drillers well completion reports in the vicinity indicate this aquifer is relatively stable over time and throughout the annual hydrological cycle compared to the shallow alluvium wells and deeper bedrock completed wells.

3.3 Water Quality

This section summarizes the information in record searches, site data, and studies in the project vicinity to summarize the groundwater quality. A high ranked site would not be proximal to private well septic systems, gasoline service stations, nor contain elevated concentrations of minerals and elements, or in such an area that would be susceptible to saltwater intrusion.

Groundwater quality in the Fort Bragg Groundwater Basin 1-021 is variable. Seawater intrusion is generally not common in the marine terrace aquifers unless in direct contact with the ocean or beach and dune deposits. The majority of marine deposit aquifers in the Fort Brag Groundwater Basin are not in direct contact with beach deposits, including that of the MUSD property, as it is well above sea level (±400-feet MSL).

High iron and sulfur reduced constituents are common in well water in the Fort Bragg Groundwater Basin area. This process of reducing iron and sulfur from the marine terrace materials generally requires various species of bacteria present and organic matter inputs. The majority of well water in the area most commonly has some resultant ferric hydroxide and less commonly and more isolated incidents of hydrogen sulfide precipitates. High concentrations of either constituent requires water treatment via filtration, settlement, or aeration processes prior to drinking.

Since the targeted aquifer here is shallow (<50 feet below the ground surface) there is a higher risk of surface contamination from septic systems, environmental spills, and fuel leaks. There are private septic systems in the vicinity, therefore; treatment via chlorine is most commonly used.

Although there is limited water quality data in the vicinity from deep bedrock wells, it is generally known that variable to elevated concentrations of manganese and iron, among other minor constituents, are encountered in irrigation, domestic and municipal wells completed into these rocks and often require additional treatment prior to consumption.

3.4 Environmental Impacts

For the proposed new supply wells, potential environmental impacts considered were based on proximity to nearby private wells, anticipated water levels, potential adverse effects to wetlands, critical habitats, creeks, or any biological resources. This study reviewed the location of new supply wells together with Site studies and habitat mapping, zoning and land use maps, coastal commission zoning, State environmental cleanup site databases and cultural or visual impacts.

Depending on the preferred well sites, some-short term noise effects may need mitigation depending on the drilling methods used and how close and how many neighbors are proximal to the construction. Shallow wells with boreholes up to 12-inches in diameter within unconsolidated materials can generally use the smaller, more agile, and quieter auger type drill rigs. Deeper boreholes that are constructing wells into hard rock generally require larger, less mobile, larger footprint to mobilize and towering-up (removing additional trees and limbs), louder rotary type drill rigs.

3.5 Well Construction Logistics and Engineering Feasibility

Several logistical and engineering factors were considered here when drilling, constructing, and preparing the new well site. The new well site should be accessible for drilling construction and for long term maintenance. The location should not be located below overhead power lines, but should have electricity nearby. The location should not be in close proximity to existing sewer lines or septic systems, excessive tree limbs (drill tower), steep slopes, or unstable ground conditions. New well sites are more economically feasible if located near existing water conveyance piping, treatment facilities. and storage tanks (discussed below).

3.6 Cost

The considerations above in the drilling feasibility and logistics also effect the overall construction costs. As stated above, if the new wells are located relatively far from existing water supply lines, treatment facilities or storage tanks this will cause pumping supply water uphill or large distances and will require significantly more power over time and pipeline construction costs to tie into existing facilities may be cost prohibitive. Other factors that may control overall costs of constructing new wells at the Site are CEQA considerations, required Site grading / preparation / improvements.

The drilling depths and conditions encountered at the time of well construction can greatly affect the overall cost and drilling methodology. For example, using 2023 dollars, a 5" diameter well casing constructed (including well development and pump testing) in unconsolidated sediments (alluvium, marine terrace, fluvial sand/gravel) is approximately \$300-400 per foot using an auger drill rig; while a deep bedrock well, constructed using larger rotary type drilling rig methods is typically in the range of \$600-800 per foot of well depth.

3.7 Well Site Screening Results

Three potential zones for wells using two types of drilling methods on the Site property on Little Lake Road were considered in this study for well siting analysis. The Sites has been visited and worked on (well drilling and geotechnical evaluations) extensively by GHD and other consultants prior and is further evaluated here using the above described criteria.

A summary of results of the scoring for Site Zones A, B, and C using shallow construction drilling methods (hollow stem auger) and deeper bedrock drilling methods (rotary) are provided below in Tables 1 and 2, respectively.

| Potential Well Site | Water Quantity | Water Quality | Environmental Impacts | Logistics & Engineering | Cost | Score | Ranking |
|-----------------------------|----------------|------------------|--------------------------|----------------------------|------|-------|---------|
| Maximum Potential Points | 30 | 20 | 20 | 15 | 15 | 100 | |
| | | Shallow W | /ell Construction (Au | uger Drilling) | | | |
| Zone A | 25 | 15 | 18 | 12 | 12 | 82 | 2 |
| Zone B | 30 | 15 | 18 | 15 | 15 | 93 | 1 |
| Zone C | 10 | 15 | 18 | 12 | 15 | 70 | 3 |
| | | Deep We | I Construction (Rota | ary Drilling) | | | |
| Zone A/B/C | 15 | 15 | 15 | 10 | 10 | 65 | 4 |

 Table 1
 Well Site Ranking Summary

3.7.1 Shallow Well Construction

Zone A

Zone A (ranked #2 here) is located in the northeastern most portion of the Site and contains two preliminary well locations (Well #9 and Well #10). This zone contains all three of the existing MUSD Wells (#1, #2 and #6) and is the most explored. Land use is primarily forested and is bordered by three residential properties (two to the north and one to the east). Specific well siting in this area together with analyzing and addressing potential impacts would be coordinated with MUSD staff. The main benefits and highlights of this zone are:

- The anticipated shallow marine terrace materials here are anticipated to be the thickest, resulting in an above average yield (based on the existing hydrogeologic conceptual model of the Site);
- Water quality (relatively good) is anticipated to be comparable to that of existing MUSD wells, however, it is unclear how close the residential septic systems to the north would be to the final well site here and how much noise mitigation would need to be considered;
- There is ample room to adjust the exact location of the test wells to provide required setbacks from any potential wetlands, springs, or other environmental considerations;
- The property is owned by MUSD and access to Zone A would require developing a new access road; and,
- The site will likely need some tree removal, and is clear of overhead power lines and is relatively close to the existing and future water supply lines, the water treatment facility, and supply tanks.

Overall, this is a good potential site for consideration of well locations. This area has the potential to include thicker marine terrace deposits compared with other areas and a saturated water bearing zone. Although there are no major issues, noise mitigation measures for adjacent residences and wetland/watercourse setbacks may be necessary.

Zone B

Zone B (ranked #1 here) starts roughly in the center of the property runs southeast across the length of the parcel. Zone B contains five preliminary well locations (Wells #7, #8, #11, #12, and #13) with Wells #7 and #8 are located on the southern half of the property and Wells #11, #12, and #13 on the northern half of the property. Land use in this zone currently includes access roads and the very topmost portion of the delineated wetlands (shown in Appendix A Figure B), and contains heavy brush and tree cover in the northern portions of the zone. Additionally located in this zone are two abandoned concrete caisson wells and the student run radio transmission facilities. The nearest private wells are located approximately 225-feet north in creek deposits, and approximately 175-feet to the east screened in bedrock. Specific well siting in this area and analyzing and addressing impacts would be coordinated with MUSD staff. The main benefits and highlights of this site are:

- The anticipated shallow marine terrace materials here would range from a size comparable/equivalent to that of MUSD Wells #1 and #2 and the caisson wells (22 feet), resulting in an above average water yield for the area (based on available site well completion reports, attached in Appendix B.
- Water quality (relatively good) is anticipated to be comparable to that of MUSD Wells #1 and #2;
- There is sufficient room to adjust the exact location of the test well away from any potential wetlands, springs, or other environmental considerations;
- The property is owned by MUSD and access to a location would require developing a new access road to access the northern three wells; and,

• The site will likely need some tree removal, and is clear of overhead power lines and has well locations relatively close to the existing and future water supply lines, and storage tanks.

Overall, this is the most suitable and broadest area for potential site test wells. This area likely includes the thickest marine terrace deposits and saturated water bearing zone and enough space to accommodate wetland setbacks and other CEQA considerations. Although there are no major issues, noise mitigation measures for adjacent residences may be necessary.

Zone C

Zone C (ranked #3 here) is located along the western portion of the property and contains two potential well locations (Well #14 and #15). Zone C likely has the thinnest marine terrace deposits and has the most uncertainty about water quantity. Land use at this site is currently unused and covered in heavy brush. The nearest private wells are is located 150 feet to the west and 225 feet to the north and is screened in bedrock. Specific well siting in this area and analyzing and addressing impacts would be coordinated with MUSD staff. The main benefits and highlights of this site are:

- There is decent room to move around the exact location of the test well away from any potential wetlands, springs, or other environmental considerations;
- The property is owned by MUSD and access to a location would require developing a new access road; and,
- The site will likely need some tree removal, and is clear of overhead power lines.

Overall, this is the most challenging location for the consideration of a test wells with the majority of the area covered in heavy brush and the potential for shallow bedrock and poor yielding wells. Additional construction considerations may include noise mitigation measures for adjacent residences and drilling rig access.

3.7.2 Deeper Well Construction Zones A/B/C

Bedrock wells (ranked #4 here) could potentially be located anywhere on the parcel due to the separation of the marine terrace aquifer and the bedrock aquifer (via a constructed well seal) and it would not hydraulicly interfere with the wells screened in the marine terrace. Ideally a bedrock well would be located as practicably far away from the nearest private well that is screened in bedrock, approximately 350 feet northeast and 440 feet northwest). However consideration needs to be made for constructability due to the size of drill rig required to drill a bedrock borehole being is significantly larger than one required for a shallow marine terrace borehole. Therefore, drill rig and construction access prioritize the location of a potential bedrock well to areas with enough room for a bedrock capable drill rig to operate. Currently the most accessible area is the southwestern corner of the property and a potentially suitable bedrock boring location is shown on Appendix A, Figure C. This area of the property is currently used for maintenance vehicle fleet parking, the maintenance shop, and access roads. Specific well siting in this area would be coordinated with MUSD staff. The main benefits and highlights of this site are:

- There is ample room to adjust the exact location of the test well away from any potential wetlands, springs, or other environmental considerations;
- The property is owned by MUSD and access to a location here would be good; and,
- The site is generally clear of overhead power lines and trees.

Overall, the Site is a relatively poor site for consideration of a bedrock test well location. The major issues include relatively poor yielding bedrock wells on adjacent properties with relatively low typical yields and much greater construction cost for a deeper, larger diameter casing, bedrock well relative to the shallow marine terrace wells. Since

it is currently unknown if a larger diameter deeper cased well could produce comparable water supply to the known marine terrace wells, it is considered here to be risky from a cost-benefit point of view.

4. General Findings and Conclusions and Recommendations

In completing the well siting study, areas around the existing properties were screened for potential yield, major flaws, and evaluated using the criteria described in Section 3.0. Site visits and Site data, well logs, and discussions with MUSD staff were part of developing the ranking scores indicated above in Table 1.

Based on the information collected during this study, and in the professional judgement of GHD's hydrogeologist, the two zones with the highest rankings for potential test well sites (Zone A and B) are the most likely to provide productive water supply wells. Zone C and bedrock well have a lower likelihood of providing a high producing water supply well, however exploratory test wells would provide more information regarding well feasibility in these areas.

These two sites scored comparably for most of the criteria with some differences in logistics and engineering (distances to pump water to the treatment facility and storage tanks, and longer distance to bring power).

5. Recommendations

Based on data collected during this study and previous reports GHD recommends the following:

- That a total of up to ten (10) new test wells be constructed, shown in Appendix A, Figure C. A total of nine (9) shallow marine terrace test wells are recommended, which should maintain an approximately 120-foot spacing to reduce the potential of well interference from neighboring wells in the anticipated radii of influence. These wells should be constructed similar to the design of MUSD Well #6 terminating at the bedrock interface. One (1) bedrock test well may be constructed where ease of access and construction considerations dictate and be constructed such that the upper marine terrace aquifer is sealed off from the lower screened sections of the well.
- 2. An initial operational plan of the new well field, in coordination with the existing MUSD wells (Well #1, Well #2 and Well #6), should maintain that no more than half of the well field (Wells #6 #7) should operate at one time and ideally no adjacent wellfield wells be pumping at the same time to reduce the potential for adverse drawdown and hydraulic interference effects. Additionally, pumping of any one well should not exceed 12 hours in a day to allow for time for aquifer recharge in the immediate areas of the pumped wells the well field. The well pumping schedule may be revised from this initial recommendation based on the actual capacity of individual wells, monitoring data, measured aquifer response, and actual future emergency water supply needs.
- The proposed well field should be pump tested during the MCCSD hydrological testing period, and in accordance with, MCCSD Ordinance 2020-1 which begins after August 20th and before a total of 6-inches of rainfall has been recorded.
- 4. Based on the relatively shallow aquifer thickness, it is recommended that wells be constructed with a reduced surface seal (20-feet in depth) with approval from the Division of Drinking Water. This reduction may result in a review from the Division of Drinking Water to determine if well water is considered Groundwater Under Direct Influence of Surface Water (GWUDI). Other wells near the Site that have a reduced surface seal are not currently considered GWUDI, however, wells considered GWUDI are required to meet surface water standards and may require additional treatment.

6. References

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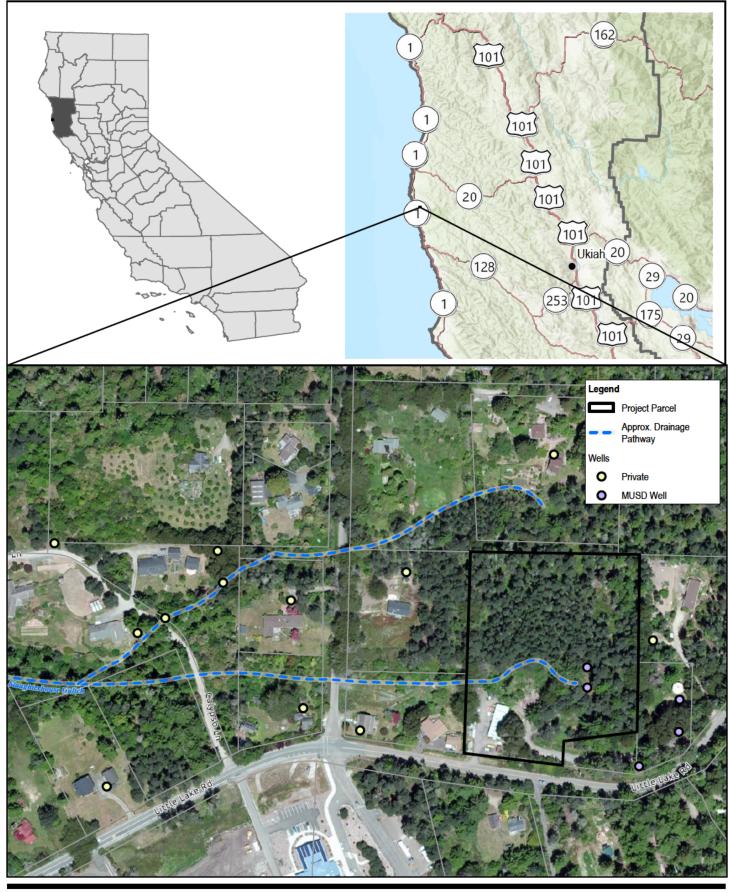
University of Montana Numerical Terradynamic Simulation Group (UMNTSG), 2015. Average annual potential evapotranspiration in mm/yr. Managed by esri. Updated August 26, 2020. ArcGIS Server URL: https://landscape6.arcgis.com/arcgis/.

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Appendices

Appendix A Figures









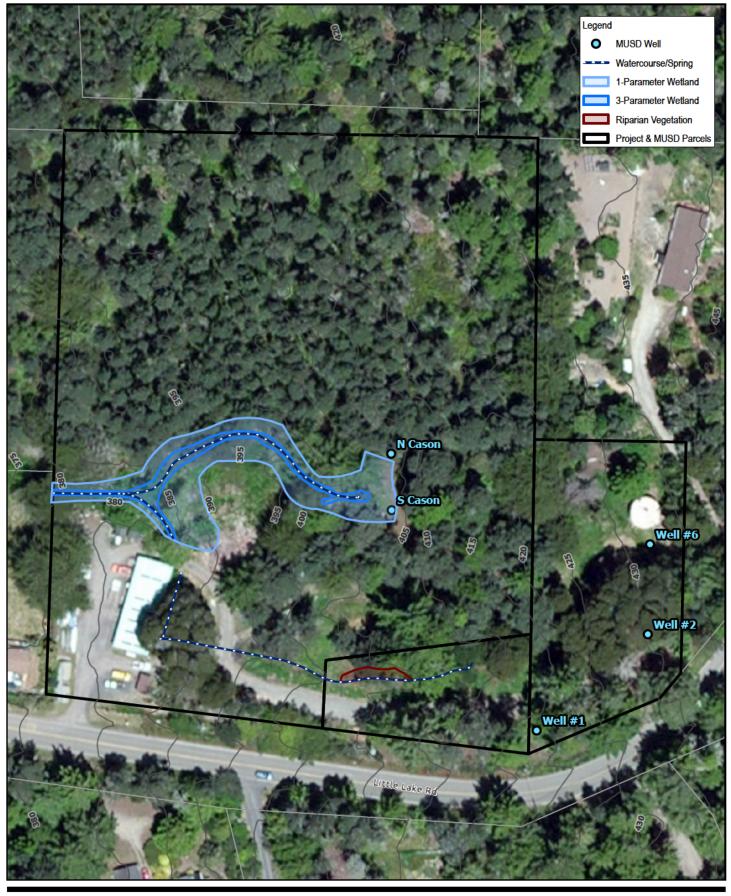
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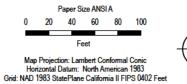
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FIGURE A

Vicinity Map

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FIGURE B

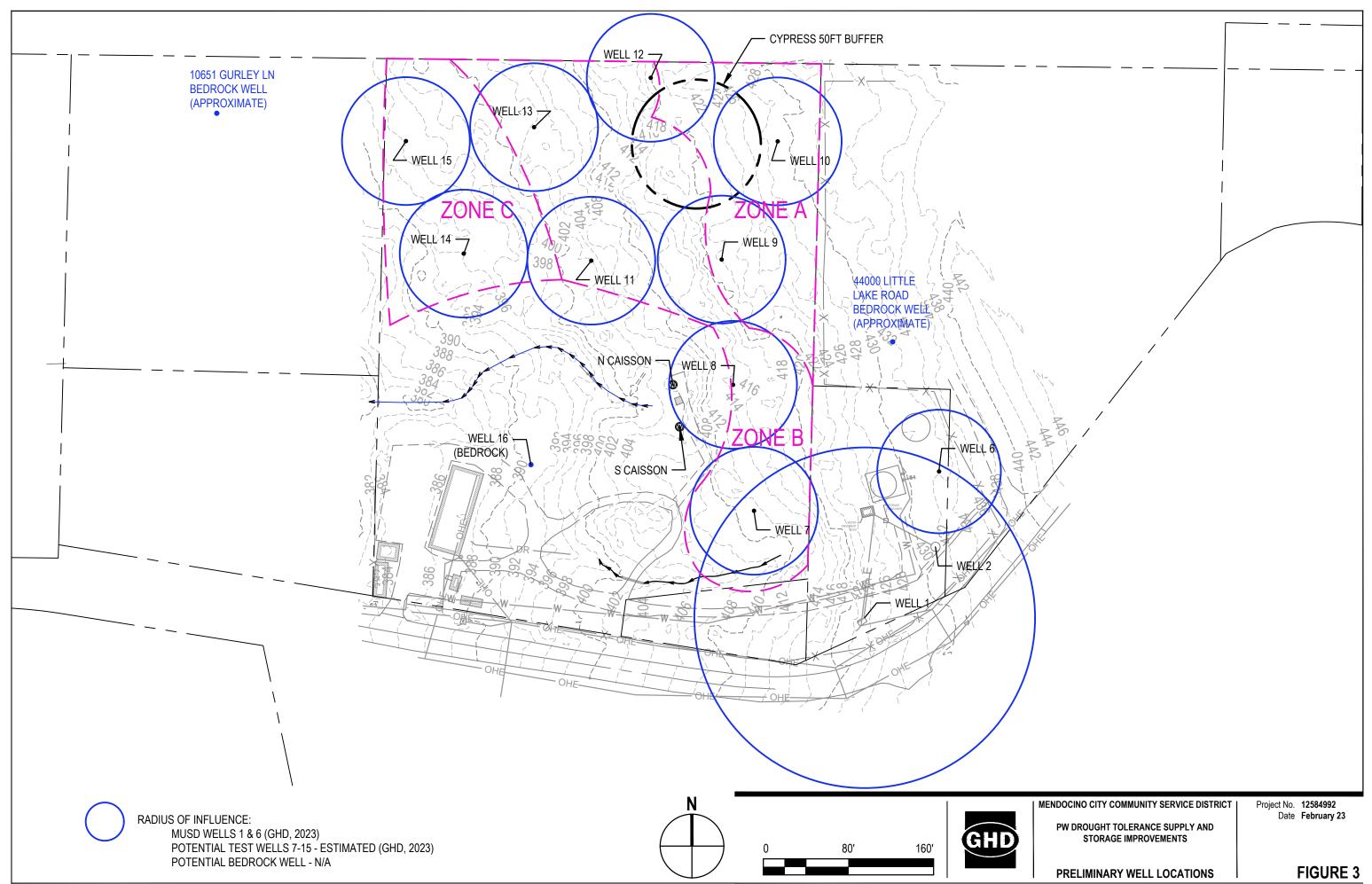
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Appendix B Well Completion Reports

State of California Well Completion Report Form DWR 188 Auto-Completed 4/19/2021 WCR2021-001445

| Owner's V | Vell Numb | er WW-6 Date Work Began 12/10/2020 Date Work Ended 12/11/2020 |
|---------------|--------------|--|
| Local Per | mit Agency | y Environmental Health Division - Fort Bragg Office |
| Secondary | y Permit A | gency Permit Number WW23932 Permit Date12/02/2020 |
| Well C | Dwner (| must remain confidential pursuant to Water Code 13752) Planned Use and Activity |
| Name | | Activity New Well |
| Mailing A | ddress | Planned Use Water Supply Domestic |
| | 76 | xxxxxxxxxxxxxxxxx |
| City I | 0000000 | State XX Zip XXXXX |
| | | Well Location |
| Address | 44020 | Little Lake RD APN 119-100-23 |
| City N | Aendodcin | o Zip 95460 County Mendocino Township 17 N |
| Latitude | 39 | 18 45.9035 N Longitude -123 46 54.1397 W Range 17 W |
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| Vertical E | 3 - | |
| 1 | Accuracy | Horizontal Datum WGS84 Elevation Accuracy Unknown Location Determination Method Unknown Elevation Determination Method |
| Location | / ceuracy | |
| | | Borehole Information Water Level and Yield of Completed Well |
| Orientatio | on Vertie | cal Specify Depth to first water 16 (Feet below surface) |
| Drilling M | lethod A | Depth to Static |
| | | Water Level 26.5 (Feet) Date Measured 12/11/2020 |
| Total Dep | oth of Borir | Ang 45 Feet Estimated Yield* 6 (GPM) Test Type Pump Test Length 8 (Hours) Total Drawdown 10.5 (feet) |
| Total Dep | oth of Com | pleted Well 45 Feet *May not be representative of a well's long term yield. |
| | | |
| | | Geologic Log - Free Form |
| Depth Surf | | Description |
| Feet to | | Description |
| 0 | 5 | Silty clay with sand (dry-soft) |
| 5 | 10 | Silty sand yellowish (dry-loose) |
| 10 | 15 | Poorly graded sand, fine sand mix |
| 15 | 20 | Graded sand light gray, fine sand |
| 20 | 25 | Well graded sand, yellowish (wet) fine-coarse sand |
| 25 | 30 | Yellowish silty sand |
| 30 | 35 | Poorly graded sand, coarse sand (wet) |
| 35 | 40 | Dark brown wethered bed rock |
| 40 | 45 | Solid bed rock |

| | | | | | | | Casing | S | | | | | | | | | | | | |
|---------------------------------------|-----------------------------------|----------------------------|-------------------|-----------|------------------|-------------------------------|--|-------------------------|-----------------------|------------------------------------|-----------------------|---------------------------------|-----------------------|--------------------|----|-------|--|--|--------------|---|
| Casing # | | m Surface o Feet | Casii | ng Type | Material | Casings | Specificatons | Wal Thickn (inche | ess | Outside Diameter (inches) | Screen Type | Slot Size if any (inches) | Desci | ription | | | | | | |
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| 2 | 25 | 40 | Scre | en | PVC | | 3 in. SDR: kness: 0.265 | 0.26 | 55 | 5.563 | Milled Slots | 0.04 | SCH 80 SCF | REEN | | | | | | |
| 3 | 40 | 45 | Blan | K | PVC | | 3 in. SDR: kness: 0.265 | 0.26 | 35 | 5.563 | | | Sch 40 Blank | ¢ | | | | | | |
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| Depth from Surface Feet to Feet | | Fill | I Fill Type Detai | | | ls | | Filter Pack Size | | | Description | | | | | | | | | |
| 0 | 18 | Ceme | ent | Portland | d Cement/Neat (| Cement | | | | | | Grout | | | | | | | | |
| 18 | 20 | Bento | nite | Non Hy | drated Bentonite | 9 | | | | | | Pellets/Time Release | | | | | | | | |
| 20 | 45 | Filter F | Pack | Other G | Fravel Pack | | | | #8 | | | Sand | | | | | | | | |
| Other | r Observa | ations: Boreho | le Sp | pecific | ations | | | | | Certific | ation S | tatement | t | | | | | | | |
| Śu | h from rface to Feet | | Bor | ehole Dia | ameter (inches) | | Name | | | CLE | AR HEART | rate to the best of DRILLING | of my knowledge a | and belief | | | | | | |
| 0 | 45 | 13 | | | | | Person, Firm or Corporation 555 B W COLLEGE AVENUE SANTA ROSA CA 95 | | | | | | 95401 | | | | | | | |
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| ATTACH ADDITIONAL INFORMATION. IF IT EXISTS. Signed Well DRILLER/AUTHORIZED REPRESENTATIVE DATE | | C-57 LICENSE NUMBER |

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STATE OF CALIFORNIA THE RESOURCES AGENCY DEPARTMENT OF WATER RESOURCES Sec. 23752 WATER WELL DRILLERS REPORT

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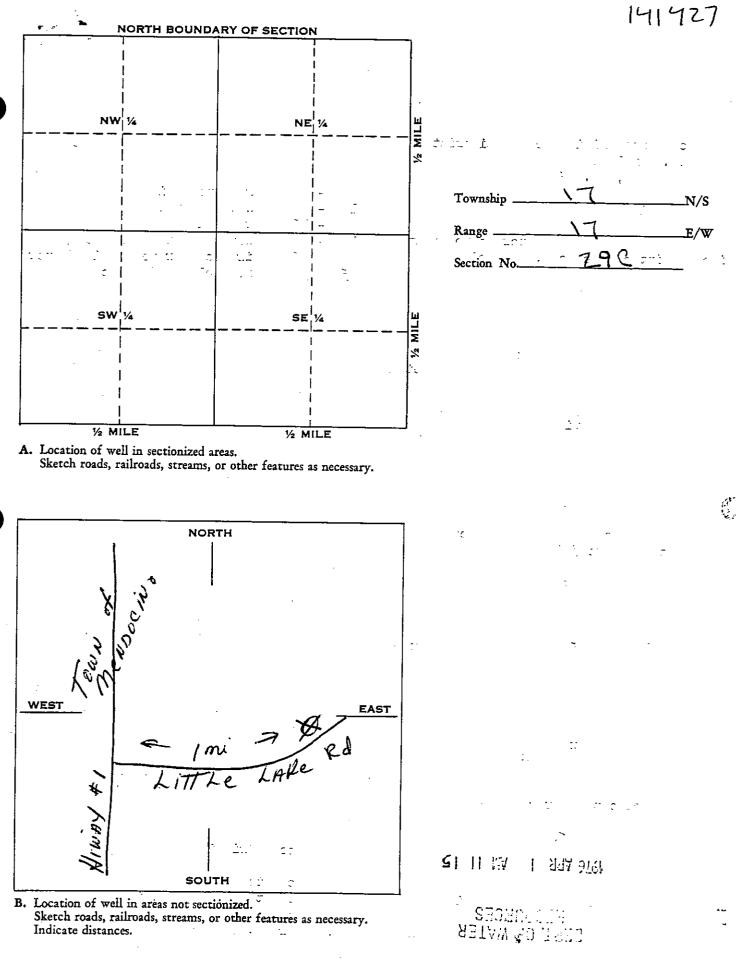
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| fr. | 1 | ít. | row | ft. | in. | x in. | | | | | | | | |
| 21 | | 36 | 5 | 2 | 1/8 | 3 x 4 | | | | | | | | |
| | | | | | | | | | | | | • | | |
| | | | | 1 | | | | | _ | | | | | |
| | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | - |
| | VST'RTI | CTION | • | | | | | | | | | | | |
| · · | | al provided? | | | fo what depth | 20 fr. | | | | | | | | |
| | | | | No X | | | , | | | | | | | |
| | | ainst pollution | | 110.00 | ar yes, note | depth of strata | 1 | | | | | | | |
| From | ft. | | <u>ft.</u> | | | | 107 . | | 3/23/ | 76,, | , Completed 3/ | 23/76 | | |
| From | ft. | | fr. | | | | Work st | | | TATEME | | | | |
| Method of sea | | cement | on gr | aver pa | ick | | | | | | NI: y jurisdiction i | and this repo | ist is true | to the her |
| (9) W A | | | | | | | | | ledge and | | , 1 | | + + + + 4 = 1 | Des |
| Depth at whi | ch water w | as first found | , if known | | ft. | | | | - | | | | | |
| Standing_ieve | l before pe | rforating, if | known | | ft. | | NAME | 3 | Weeks | | ing and . | | | |
| Standing leve | l after perf | forsting_and o | developing | • (|) ít. | | 4 | | | | m, or corporation) | (1) ped or p | riniea } | ~ · |
| (10) W | ELL TI | ESTS: | | | | | Addres | 55 | Sebas | topol | | | | []] |
| Was pump tes | t made? Y | ies 💭 🛛 No | | f yes, by whom |) bail | | | | Sebas | topol. | Californ | <u>11a 9,547</u> | 70 Je / | Will |
| a: 30 | 2 | al./min. with | 22 | ft, drawdo | wn after | hrs. | [SIGNE | :D] | Geral | d Thom | pson | Aller | the | <u> </u> |
| aperature | of water (| cold | Was a chemie | al analysis mad | le? Yes 🗍 1 | vo 🕱 | By: | | Marv | E Tho | mpsón ^{(Vell Dril} | 2) / [[000 | <u> </u> | |
| Aperature of water CO d Was a chemical analysis made? Yes. No X | | | | | | | | | יסי | 2681 | Dated Ma | rch 24 | | 19 76 |

SKETCH LOCATION OF WELL ON REVERSE SIDE

WELL LOCATION SKETCH



| REGIONAL WATER POLLUTION CONTROL BOARD No. 1 THE RESOURCES Defit abpropriate number) THE RESOURCES | S AGENCY OF CALIFORNIA S AGENCY OF CALIFORNIA |
|--|---|
| OWNER: | |
| Nam | (11) WELL LOG: |
| Addı | Total depth 20 ft. Depth of completed well a Soc. 1 |
| <u>Auu</u> | |
| <u> </u> | $= 12 \cdot 13 \cdot gravel$ |
| (2) LOCATION OF WELL: | <u>13 ° 22 vellow clay</u> |
| County Mendocino Owner's number, if any- | 22 " 29 shale and rock |
| R. F. D. or Street No. map attached | Two identical wells side by side |
| • | |
| | uu |
| | |
| (3) TYPE OF WORK (cbeck): | |
| | |
| New well g Deepening Reconditioning Abandon If abandonment, describe material and procedure in Item 11. | |
| (4) PROPOSED USE (cbeck): (5) EQUIPMEN | $- - \qquad N \in \mathbb{R}^{3}$ $- $ |
| | $\overline{\mathbf{x}}$ |
| Irrigation 🗌 Test Well 🗍 Other | |
| Dug Well | a av in shead water tank. |
| (6) CASING INSTALLED: If gravel packed | school water tank. |
| SINGLE DOUBLE | |
| From ft. to ft. Diam. Wall of Bore ft. | |
| 36" concrete casing 60" 0 | 30' |
| | |
| | |
| <u> </u> | |
| Type and size of shoe or weil ring none Size of gravel: 13 inc | h New Rel Hiway |
| Describe joint slip | |
| (7) PERFORATIONS: | |
| | |
| Size of perforations | |
| From ft. to ft. Perf. per row Rows t | <u>in.</u> in |
| bottom 6 ¹ Kows r | mendo. City |
| <u>и и и</u> ини и | |
| | ····· |
| | Hiway 28 |
| (8) CONSTRUCTION: | |
| Was a surface sanitary seal provided? X Yes I No To what depth | |
| Were any strata sealed against pollucion? I Yes 👳 No If yes, note depth of strata | |
| From ft. to ft. | FOR OFFICIAL USE ONLY |
| Method of Sealing | |
| | Work started 10/14/63 19 . Completed 10/18/63 1 |
| (9) WATER LEVELS: | WELL DRILLER'S STATEMENT: |
| | This well was drilled under my jurisdiction and this defait is true to the l my knowledge and belief. |
| anding level before perforating 12 | 2 ft. NAME D & D D + 11 in - |
| | 2 fr. (Person, firm, or corporation) (Typed or printed) |
| (10) WELL TESTS: | Address RT. 1 Box 617-H |
| Was a pump test made? Thes X No If yes, by whom? | Ukiah, California |
| | ISIGNED] Nalph Burn |

87649 5-68 25M QUIN () A SPO

DWR 188 (REV. 3-54)

| | · · · · · · · · · · · · · · · · · · · | | | • |
|-----|--|---|---|---|
| | ORIGINAL | STATE OF C | ALIFORNIA | Do not fill in |
| | · 、 | THE RESOUR | • | |
| | File with DWR | DEPARTMENT OF V | ATER RESOURCES | No. 140367 |
| (| e of Intent No | WATER WELL D | RILLERS REPORT | |
| | Local Fermit No. or Date 8002 replace | ces #7721 | | State Well No. |
| | | | 090-004 | Other Well No. TIVITYG7D |
| | (1) | | (12) WELL LOG: Total | depth_59_ft. Depth of completed well_60_ft. |
| | Addre | | from ft. to ft. Formation (I | Describe by color, character, size or material) |
| | City | | 0 - 12 Brown | |
| | (2) LOCATION OF WELL (See in | structions). | <u>12 - 15 White</u> | sandy clay |
| | (2) LOCATION OF WELL (See in County | ner's Well Armber 19-090-04 | <u>+ 15 - 20 Blue</u> | |
| | Well address if different from aboveUODU | Gurley Lane | <u>20 - 29 Black</u> | |
| | Township Mendocino Range A 9546 | 0Section | 29 - 59 Blue | and block rock |
| | Distance from cities, roads, railroads, fences, etc | | | |
| | | | | |
| | | · · · · · · · · · · · · · · · · · · · | | |
| | A LIDI IN | | | |
| | BUBLEV GAL | (3) TYPE OF WORK: | \mathcal{R} | |
| Ļ | .70 | New Well 🔀 Deepening 🗌 | | <u>^</u> |
| • | | Reconstruction | - | |
| 4 | WETL Y | Reconditioning | <u> C</u> | |
| ١ | (f) | Horizontal Well | 5110 - 1 161 | |
| | 1 I ALF | Destruction (Describe destruction materials and | | |
| | from | procedures in Item 12 | | |
| `: | | (4) PROPOSED USE | | |
| | MAN IN | Domestic | <u> </u> | |
| | 191161 | | | <u> </u> |
| (| Part - | Industrial | <u>, ~ \0}-~</u> | |
| | | Test Well | $AH \sim - \circ$ | · |
| | | Stock | | ····· |
| | · · · · · · · · · · · · · · · · · · · | | | |
| | (5) EQUIPMENT: (6) GR | Other | | · · · · · · · · · · · · · · · · · · · |
| - | | AVEL PACK: | | |
| | Rotary Reverse Kark | of home 26 and 0 | | |
| | Other D Bucket X Packed | 20 50 | | |
| | | FORATIONS: | | |
| | | perification or size of screen | <u> </u> | |
| | | | | |
| | from t. To Dia. Gage From From ft. Wall ft. | To ft. | - | |
| •. | 1 ft. above grd. 20 | 59 1 8" | | |
| . ' | 59 5 1: | | | |
| | | | _ | |
| | (9) WELL SEAL: | - Ho | | |
| | Was surface sanitary seal provided? Yes X N | o [] If yes, to depthft. | | |
| | Were strata sealed against pollution? Yes | No X Intervalft. | _ | ······································ |
| | Method of sealing COLICIE CE | | Work started May 16, 19. | 88 Completed Jula v 25 19 88 |
| | (10) WATER LEVELS: Depth of first water, if known 20 | | WELL DRILLER'S STATE | MENT: |
| | Depth of first water, if known 20 Standing level after well completion | ft. | This well was drilled under my ju knowledge and beliet | urisdiction and this report is true to the best of my |
| | (11) WELL TESTS: | nt. | SIGNEDMM_// | "Wiman |
| | Was well test made? Yes 🛃 No 🖂 If y | es, by whom? Driller | | (Well Driller) |
| | Type of test Pump 🖂 🛛 Baile | erX Air lift 🗌 | NAME Murray Well | |
| (| Booth to water at start of testft. harge $\frac{41}{2}$ gal/min after 3 hours | At end of testft | Address 30520 Sherw | or corporation) (Typed or printed) |
| 4 | | • · · · | city Fort Bragg, | |
| | | es, by whom?es, attach copy to this report | License No. 268792 | Date of this report_1)ne_25_1088 |
| | | SPACE IS NEEDED, USE N | | |
| | - ABBITIONAL | | | |

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| OWNER'S WELL No. 4796 Date Work Began 8/19/02 Ended 8/19/02 Local Permit Agency Mendocino Permit No. 15481 Permit Date GEOLOGIC LOC ORIENTATION Vertical | 7-22-2002 Degree of Angle | 807026 | DWR USE ONLY DO NOT FILL IN | |
|---|---|--|--|---|
| DEPTH FROM DEPTH TO FIRST WATER . SURFACE | (ft.) BELOW SURFACE | E | | |
| | RIPTION | | | |
| 0 2 topsoil | | | | |
| 2 20 brown clay | | | County Mendocino | |
| 20 30 weathered sandstone 30 140 sandstone | ···· | | Page 050Parcel 43 | |
| 30 140 sandstone 140 160 shale w/clay | | | | |
| | | or Latitude | NORTH Longitude WEST SecLOCATION SKETCH | |
| | | | | |
| | | ACTIVITY NEW | VWELL PLANNED USE(S) Domestic Water | |
| TOTAL DEPTH OF BORING 160 (Feet) | | | | |
| TOTAL DEPTH OF COMPLETED WELL 160 (| Feet) | *May not be represe | entative of a well's long-term yield. | |
| 0 | .F480_PVC | Gauge Slot size | DEPTH ANNULAR MATERIAL ROM SURFACE Filter Pack Ft. To Ft. Seal Material (Type / Size) 0 20 Bentonite 20 | |
| Attachments | : | | | — |
| | AME (PERSON, FIRM, OR 5001 Gravenst gned Dale Theiss | this report is complete an CORPORATION: (TYP ein Hwy No. 14.0 V [DU2 BIC] | nd accurate to the best of my knowledge and belief. Bros. Drilling, Inc. PED OR PRINTED) Sebastopol CA 95472 399220 | 6 |

| ORIGINAL File with DWF | | WELL COMPI | F CALIFOR LETIO | N REPORT | | 11124 | O NOT FILL IN |
|---|---------------------------------------|--|----------------------|---|--|--------------------------|--|
| Page of | -2 | • | · 7031 | | | | |
| Owner's Well Date Work Beg | | . Ended 122/00 | 1031 | | LATITUDE | | |
| Local Permit | Agencynedocin | O CO. CAVIRONN | vatal | Health | | | |
| Permit No. | 10395 | Permit Date | 1171 | 00 | | APN/TRS/OT | HER |
| | CEOLOGIC | | <u> </u> | | | |] |
| ORIENTATION (| DRILLING ROTA | HORIZONTAL ANGLE | | | | | ĺ |
| DEPTH FROM SURFACE | | $\underline{RY}_{\text{FLUID}} \underline{NO}$ | ve | | | | |
| Ft. to Ft. | | erial, grain size, color, etc. | , ¹ - | | | INTON . | ~ ~ |
| 01 | DRIFT | | · · · · A | Address 4375 | 5 244 | ELAK | E KOAD |
| 1 2- | SAND FIL | VE BROWN | | Tity MEND | <u>ocino</u> | | |
| 27 24 | Sand GI | RAY CRAFT | | County MEND | | urcel /3 | |
| 927 02 3 | <u>0 0440310</u> | NE GIVIY | · 1 | PN, Book | | | · [|
| | · · · · · · | | · • | Cownship | Q | ection ongitude | WEST |
| 1 | | | · · · | DEG, MIN | SEC. TION SKETCH — | UE DE | G. MIN. SEC. - ACTIVITY (∠) — |
| | | | | Ha Ici | NORTH | | NEW WELL |
| 1 | i | · · · · · · · · · · · · · · · · · · · | | contre au | | _ F ∧ | ODIFICATION/REPAIR |
| | | · · · · · · · · · · · · · · · · · · · | | WEL | | | Deepen Other (Specify) |
| | | · · · · · · · · · · · · · · · · · · · | | - | -6 | - | |
| | | 1 | | |] | - | DESTROY (Describe Procedures and Materials Under "GEOLOGIC LOG") |
| 1 | | | | N D | rive way | | PLANNED USES (\leq) |
| | 1 | | | Howse | | ¥ | ATED SUPPLY |
| ······ | | | | E | | 19 19 | Irrigation Industrial |
| | | | MESI | | | EAS | MONITORING |
| | | | | | | | ATHODIC PROTECTION |
| | | ····· | | | | | HEAT EXCHANGE |
| | · · · · · · · · · · · · · · · · · · · | | | | i | | DIRECT PUSH |
| | · · · · · · · · · · · · · · · · · · · | ····· | | | • | | |
| 1 | ····· | · · · · · · · · · · · · · · · · · · · | | | - SOUTH | | SPARGING REMEDIATION |
| | | | ······ | Illustrate or Describe Dist Fences, Rivers, etc. and a | tance of Well from Roads, ttach a map. Use additiona ACCURATE & COMPLE | Buildings, 1 paper if | OTHER (SPECIFY) |
| | · · · · · · · · · · · · · · · · · · · | | · , | | | | |
| | 1 1 | ····· | | | EVEL & YIELD O | | TED WELL |
| | | | | DEPTH TO FIRST WAT | ER (Ft.) BELC | W SURFACE | option |
| 1 | | | | WATER LEVEL | 4 (FI.) & DATE M | | 240 |
| TOTAL DEDTL | OF BORING 035 | Г | | 1 m | | ST TYPE AI | |
| | OF COMPLETED WELL | | | TEST LENGTH <u>3</u> . | . (Hrs.) TOTAL DRAWDC tative_of_a_zvell's_long- | | (Ft.) |
| | | | | | the cost of the speed strong- | crini yicut. | |
| DEPTH FROM SURFAC | BORE- | CASING (S) | | | DEPTH | ANNUI | LAR MATERIAL |
| | | MATERIAL / INTERNAL | GAUGE | SLOT SIZE | ······ | CE- BEN- | |
| Ft. to Ft. | DIA. (Inches) NUT H | GRADE DIAMETER (Inches) | OR WALL THICKNESS | IF ANY (Inches) | FL to FL I | | 『LL FILTER PACK (TYPE/SIZE) 소) |
| 1 60 | | PVC 5" | CL200 | 5 | | \mathbf{Z} | =/ |
| 60:23 | | PVC 5" | CLOO | | 27 235 | | X #3 LONE |
| 1 | | | | | | | STAR |
| , <u>, , , , , , , , , , , , , , , , , , </u> | | | : | | | <u> </u> | |
| · · · · · · · · · · · · · · · · · · · | | | | | | | |
| / АТТ | ACHMENTS (∠) | <u> </u> | | - CERTIFICATIO | ON STATEMENT | | |
| | Nogic Log | I, the undersigned, ce | nify that this | report is complete a | nd accurate to the be | | wiedge and belief. |
| N | Construction Diagram | NAME WEST-S | | DRILLING | - CO. I | \sim | |
| | physical Log(s) | IPERSON, FIRM, UPC C | EARL | DRIVE | FORT | <u> </u> | N 951127 |
| | Water Chemical Analyses | ADDRESS | | - UNITE | | <u> </u> | TATE ZIP |
| | | - 1 bal | Zan | | 12 | 114/00 | 184181 |
| · · | NAL INFORMATION, IF IT EXIST | WELL DRILLER/AUTHO | | | | SIGNED | C-57 LICENSE NUMBER |
| DWR 188 REV. 11-97 | IF ADD | ITIONAL SPACE IS NEEDED, | USE NEXT | CONSECUTIVELY N | UMBERED FORM | , | |

| | STAT | E OF CALIFORNIA | DWR USE ONLY DO NOT FILL IN |
|---|---|--|--|
| OWNER'S WELL No. 4510 | WELL COM | PLETION REPOR | T [17N17W3] |
| | No. | 762471 | STATE WELL NO. STATION NO. |
| Date Work Began 7/3/01 Ended 7/3/0 | 1 | 102411 | |
| Local Permit Agency Mendocino | | | LATITUDE LONGITUDE |
| Permit Da | te 6/15/2001 | | |
| GEOLOGIC L | | | |
| ORIENTATION Vertical | Degree of Angle | | |
| | | | |
| SURFACE | ((II.) BELOW SUP | (FAGE | |
| | CRIPTION | | |
| 0 2 topsoil | | Address 9301.N | 1. Hwy.1. |
| 2 25 brown sandy clay | | | County Mendocino |
| 25 120 soft sandstone | | | Page 340 |
| 120 190 hard sandstone | | er | Range |
| 190 220 shale & clay | <u> </u> | or . | - |
| | | Latitude | Min. Sec. Deg. Min. Sec. |
| | | | Ain. Sec. Deg. Min. Sec. |
| | | | |
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| | | | |
| | | | EW WELL PLANNED USE(S) Domestic Water |
| | | DRILLING METH | |
| | | DEPTH OF STAT | IC 26 (Ft.) & DATE MEASURED Jul.3, 2001 |
| | | WATER LEVEL | |
| | | | LD * .15. (G.P.M.) & TEST TYPEAitlift |
| TOTAL DEPTH OF BORING 220 (Feet) | | TEST LENGTH. | |
| TOTAL DEPTH OF COMPLETED WELL , 220. | , (Feet) | "May not be repre | esentative of a well's long-term yield. |
| DEPTH BORE- | CASING | | DEPTH ANNULAR MATERIAL |
| FROM SURFACE HOLE Ft. To Ft. DIA. TYPE | | Dia Gauga Alataira | FROM SURFACE Filter Pack |
| , | | Dia. Gauge Slot size | Ft. To Ft. Seal Material (Type / Size) |
| | | <u>5 160</u> | |
| | | 5 | |
| | ti7999tY.Se | | |
| | *************************************** | | , 1998, 1997 |
| | ********* | | |
| | | | |
| Attachments | 1, the undersigned, certif | y that this report is complete | ATION STATEMENT e and accurate to the best of my knowledge and belief. |
| | NAME | | Bros. Drilling, Inc. |
| | | N, OR CORPORATION) (T Venstein Hww No | |
| Geophysical Logs | | · · / | Sebastopol |
| | Signed Dale Theiss | Carol Hugs | |
| no Other | WELL DRILLER | AUTHORIZED REPRÉSE | ENTATIVE DATE SIGNED C- 57 LICENSE NUMBER |

| .) | | A | WELL COMP | LETION REPORT | | |
|--|---|--|--|---|----------------------------------|--|
| | Began | 9/9/05 Ended 1 | 9/9/05 | 0924893 | LATITUDE LONGITUDE | TT |
| | | WENDOCIN | | | | |
| Permit No | WW20 | 1432 Perm | nit Date 8-16-2005 | | WELL OWNER | |
| RIENTAT | | GEOLOG | IC LOG | | | |
| | | | | | | |
| SURF | | | ATER (n.) BELOW SURI | ACE | CA 9 | 4942 |
| Fl. | FL | | DESCRIPTION | | CATION | |
| | | toposil | | Address 1065 | GURLEY LANE | 0 |
| 0 | 2 | topsoil | | City MENDOCI | NO County MENDOCIN | A |
| 2 | 25 | brown cla | greenstone | Apr Book 110 | Page 100 | |
| 20 | | | e w/ shale | Township | Range Section | |
| 25 | 140 | greenscon | e w/ share | Latitude | NORTH Longitude | WEST |
| | | | | Deg. M | In. Sec. LOCATION SKETCH | |
| | | | | | | |
| | | | | | | |
| | | | | DRILLING METHO | | |
| | | | | | D ROTARY AIR FLUID Benton: | ite |
| | | | | DRILLING METHO DEPTH OF STATIO WATER LEVEL | D ROTARY AIR FLUID Benton: | ite 2005 |
| | H OF BC |)RING 140 (Fe | et) | DRILLING METHO DEPTH OF STATIO WATER LEVEL | D ROTARY AIR FLUID Benton: 20 | ite 2005 |
| | | DRING 140 (Fea | | DRILLING METHO DEPTH OF STATIO WATER LEVEL ESTIMATED YIEL TEST LENGTH. | D ROTARY AIR FLUID Benton: 20 | ite 2005 |
| L DEPTH | H OF CO | | 140. (Feet) | DRILLING METHO DEPTH OF STATIO WATER LEVEL ESTIMATED YIEL TEST LENGTH. | D ROTARY AIR FLUID Benton: 20 | ite 2005 1t(FT.) |
| DEPTH M SURF | HOF CO | MPLETED WELL | 140. (Feet) CASING | DRILLING METHO DEPTH OF STATIO WATER LEVEL ESTIMATED YIEL TEST LENGTH. *May not be repres | D ROTARY AIR FLUID Benton: 20 | ite 2005 [t |
| L DEPTH DEPTH M SURF/ TO F | ACE BO L DI | MPLETED WELL RE DLE A. TYPE | 140 (Feet) CASING Material / Grade Di | DRILLING METHO DEPTH OF STATIO WATER LEVEL ESTIMATED YIEL TEST LENGTH. "May not be repres | D ROTARY AIR FLUID Benton: 20 | 1te 2005 1t (FT.) AL Pack |
| L DEPTH DEPTH M SURFA TO FI 20 | HOFCO ACE HO L DI | MPLETED WELL RE LLE A. TYPE <u>5/8</u> Blank | 140. (Feet) CASING Material / Grade Di F480_PVC | DRILLING METHO DEPTH OF STATIO WATER LEVEL ESTIMATED YIEL TEST LENGTH. "May not be represent a. Gauge Stot size | D ROTARY AIR FLUID Benton: 20 | Lte 2005 Lt (FT.) AL Pack Size) |
| L DEPTH DEPTH M SURFA To FI 20 40 | H OF CO ACE HO L DI 10 | MPLETED WELL RE DLE A. TYPE 5/8 | 140. (Feet) CASING Material / Grade Di F480 PVC | DRILLING METHO DEPTH OF STATIO WATER LEVEL ESTIMATED YIEL TEST LENGTH. *May not be represent a. Gauge Slot size 160 | D ROTARY AIR FLUID Benton: 20 | ite 2005 (FT.) AL Pack Size) |
| L DEPTH DEPTH M SURFA TO FI 20 | H OF CO ACE HO L DI 10 | MPLETED WELL RE DLE A. TYPE 5/8 | 140. (Feet) CASING Material / Grade Di F480 PVC | DRILLING METHO DEPTH OF STATIO WATER LEVEL ESTIMATED YIEL TEST LENGTH. "May not be represent a. Gauge Stot size | D ROTARY AIR FLUID Benton: 20 | ite 2005 (FT.) AL Pack Size) |
| L DEPTH DEPTH M SURFA To FI 20 40 | H OF CO ACE HO L DI 10 | MPLETED WELL RE DLE A. TYPE 5/8 | 140. (Feet) CASING Material / Grade Di F480 PVC | DRILLING METHO DEPTH OF STATIO WATER LEVEL ESTIMATED YIEL TEST LENGTH. *May not be represent a. Gauge Slot size 160 | D ROTARY AIR FLUID Benton: 20 | AL Pack Size) |
| DEPTH DEPTH M SURFA TO FI 20 40 | H OF CO ACE HO L DI 10 | MPLETED WELL RE DLE A. TYPE 5/8 | 140. (Feet) CASING Material / Grade Di F480 PVC | DRILLING METHO DEPTH OF STATIO WATER LEVEL ESTIMATED YIEL TEST LENGTH. *May not be represent a. Gauge Slot size 160 | D ROTARY AIR FLUID Benton: 20 | ite 2005 (FT.) AL Pack Size) |
| AL DEPTH DEPTH M SURFA TO FI 20 40 | H OF CO ACE HO L DI 10 8.3 | MPLETED WELL | 140. (Feet) CASING Material / Grade Di F480 PVC S F480 PVC S F480 PVC S | DRILLING METHO DEPTH OF STATIO WATER LEVEL ESTIMATED YIEL TEST LENGTH. "May not be represent a. Gauge Slot size 160. 160. 200. Factor | D ROTARY AIR FLUID Benton: 20 | ite 2005 Et AL Pack Size) |
| DEPTH M SURF/ To FI 20 40 40 | H OF CO ACE HO L DI 10 8.3 1 | MPLETED WELL | 140. (Feet) CASING Material / Grade Di F480 PVC S F480 PVC S F480 PVC S | DRILLING METHO DEPTH OF STATIO WATER LEVEL ESTIMATED YIEL TEST LENGTH. "May not be represent a. Gauge Slot size 160. 160. 200. Factor | D ROTARY AIR FLUID Benton: 20 | ite 2005 Et AL Pack Size) |
| AL DEPTH DEPTH M SURF/ To Fi 20 40 40 140 | H OF CO ACE HO 10 8.3 1. 7.1 Attachm jic Log | MPLETED WELL | 140. (Feet) CASING Material / Grade Di F480 PVC S F480 | DRILLING METHO DEPTH OF STATIO WATER LEVEL ESTIMATED YIEL TEST LENGTH. "May not be represent a. Gauge Slot size 160. | D ROTARY AIR FLUID Benton: 20 | ite 2005 (FT.) AL Pack Size) |
| L DEPTH DEPTH M SURF/ To F 20 40 40 140 | H OF CO ACE HO L DI 10 8 3 17.1 Attachim jic Log construc | MPLETED WELL | 140. (Feet) CASING Material / Grade Di F480_PVC F480_PVC F480_PVC F480_PVC F480_PVC F480_PVC | DRILLING METHO DEPTH OF STATIO WATER LEVEL ESTIMATED YIEL TEST LENGTH. "May not be represent a. Gauge Stot size 160. 200. Factor CERTIFIC/ hat this report is complete FISCH BROSON (TY) | D ROTARY AIR FLUID Benton: 20 | ite 2005 (FT.) AL Pack Size) rgl |
| L DEPTH DEPTH M SURF/ To Fi 20 40 40 | H OF CO ACE BO I DI 10 8.3 1 | MPLETED WELL | 140. (Feet) CASING Material / Grade Di F480_PVC F480_PVC F480_PVC F480_PVC F480_PVC F480_PVC | DRILLING METHO DEPTH OF STATIO WATER LEVEL ESTIMATED YIEL TEST LENGTH. "May not be represent a. Gauge Slot size 160. | D ROTARY AIR FLUID Benton: 20 | ite 2005 (FT.) AL Pack Size) rgl |



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